



Mechanical Oscillations in 2D Collective Cell Migration: The Elastic Turbulence

Ivana Pajic-Lijakovic* and Milan Milivojevic

Department of Chemical Engineering, Faculty of Technology and Metallurgy, University of Belgrade, Belgrade, Serbia

Various types of mechanical waves, such as propagative waves and standing waves, are observed during 2D collective cell migration. Propagative waves are generated during monolayer free expansion, whereas standing waves are generated during swirling motion of a confluent monolayer. Significant attempts have been made to describe the main characteristics of mechanical waves obtained within various experimental systems. However, much less attention is paid to correlate the viscoelasticity with the generated oscillatory instabilities. Mechanical waves have recognized during flow of various viscoelastic systems under low Reynolds number and called “the elastic turbulence.” In addition to Reynolds number, Weissenberg number is needed for characterizing the elastic turbulence. The viscoelastic resistive force generated during collective cell migration caused by a residual stress accumulation is capable of inducing apparent inertial effects by balancing with other forces such as the surface tension force, the traction force, and the resultant force responsible for cell migration. The resultant force represents a product of various biochemical processes such as cell signaling and gene expression. The force balance induces (1) forward flow and backward flow in the direction of cell migration as characteristics of the propagative waves and (2) inflow and outflow perpendicular to the direction of migration as characteristics of the standing waves. The apparent inertial effects are essential for appearing the elastic turbulence and represent the characteristic of (1) the backward flow during the monolayer free expansion and (2) the inflow during the cell swirling motion within a confluent monolayer.

Keywords: multi scale nature of viscoelasticity of multicellular system, collective cell migration, apparent inertia effects, the elastic turbulence, rheological behavior of extracellular matrix

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*Correspondence:

Ivana Pajic-Lijakovic
iva@tmf.bg.ac.rs

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INTRODUCTION

Collective cell migration within a monolayer induces spontaneous generation of mechanical waves [1–5]. A more comprehensive account of oscillatory patterns generation is essential for a wide range of biological processes such as morphogenesis, wound healing, regeneration, and cancer invasion [6–9]. Specifically, in this review, we concentrate on mechanical oscillations, a term we use to identify all periodical fluctuations of mechanical parameters, such as cell velocity, the resulting strain, substrate tractions, and stresses. These oscillations can be divided into two major categories: (1) standing waves generated in a confined environment [3, 5, 10–12] and (2) propagative waves generated during monolayer free expansion that travel through the system [2, 5, 13]. The standing waves represent a characteristic of local cell rearrangement, which leads to swirling motion [3]. Propagative waves have been observed during wound healing [2]. This monolayer expansion

induces fluctuations of cell packing density [13]. Tlili et al. [13] reported that the frequency of velocity waves depends only on cell packing density at the moving forward. Both types of waves induce a periodical softening and stiffening of multicellular domains [2, 3, 5]. It is necessary to correlate cell packing density with cell strains and residual stress accumulation.

Oscillator, wave-like motion of multicellular systems has been related to long-time effective inertia [3, 11]. The effective inertia is induced by generated cellular stress during long-time rearrangement. Notbohm et al. [3] considered a cell stress generation as a product of a chemical coupling where cellular stress results in increased contractility, which has a feedback impact to the effective inertia. The effective inertia, together with cellular elasticity, supports the oscillatory waves of motion [3]. Serra-Picamal et al. [2] assumed a biphasic stress response of single cells as a product of cytoskeletal reinforcement and fluidization. They also neglected long-time inertial effects. Banerjee et al. [14] coupled local strain with contractility and impose a turnover time for contractile elements, resulting in effective inertia and viscoelasticity based on the formulated continuum model. They did not take into consideration stress relaxation and residual stress accumulation caused by collective cell migration. Murray et al. [15] related cell packing density with cell stress. They also neglected inertial effects. Various approaches have been applied. Notbohm et al. [3] proposed a continuum model formulated in terms of a few coarse-grained fields such as traction and velocity, measured directly in the experiments. Murray et al. [15] proposed a continuum model presented as a system of equations capable for describing interrelation between variables such as (1) cell packing density, (2) matrix density, and (3) matrix viscoelasticity. Serra-Picamal et al. [2] and Deforet et al. [11] formulated stochastic particle-based simulations. Serra-Picamal et al. [2] balanced active propulsion force with cell elastic force and cell–matrix friction force. Deforet et al. [11] accounted for the force of inertia and balanced it with friction, intercellular adhesions, and active propulsion.

Significant attempts have been made to describe the main characteristics of mechanical waves by considering various types of experimental systems. The main characteristics of standing waves are (1) the radial velocity and cell tractions are uncorrelated; (2) radial stress component σ_{crr} and the corresponding strain rate $\dot{\epsilon}_{crr}$ are uncorrelated; (3) radial stress component is simultaneously tensional and compressional; and (4) time derivative of the stress component is in a phase with the corresponding strain rate [3]. The main characteristics of propagative waves are that (1) normal stress component σ_{cxx} and corresponding strain rate $\dot{\epsilon}_{cxx}$ are in phase quadrature, (2) normal stress component is always tensional, and (3) velocity and cell tractions are uncorrelated [2]. Even though the most studied model is Madin-Darby canine kidney cells (MDCK), other types have been employed, and despite the intrinsic variability between them, all reports seem to agree on the typical times and space scale: mechanical oscillations happen with a periodicity of ~ 0.5 – 1 mm and ~ 3 – 6 h [2, 3, 5]. The effective velocity of transmission of mechanical signals, whether traveling or standing waves, is 0.2 – 1 $\mu\text{m}/\text{min}$ [2, 3]. These cooperative motions are driven by active cellular forces, but the physical nature of these forces

and how they generate elastic waves remain poorly understood. However, it is well-known that generation of waves and their transfer strongly depends on the state of cell–cell junctions and contractility [2, 3, 16, 17]. Most of the works on generation of mechanical waves within cell monolayers have been carried out on fibroblasts, which develop weaker cell–cell adhesions [5]. The knowledge obtained on these cell types is difficult to transfer on epithelial cells, which develop strong cell–cell junctions. However, various confluent multicellular systems under *in vivo* conditions are capable of generating the cell swirling motion and on that base mechanical waves, which have been experimentally confirmed [18, 19]. Additional experimental work is necessary to correlate the state of cell–cell adhesion contacts and the characteristics of mechanical waves. Until now, little is reported about influence of the monolayer viscoelasticity on propagation of mechanical waves. Tambe et al. [1], Serra-Picamal et al. [2], and Notbohm et al. [3] treated a monolayer as homogeneous, isotropic, and elastic. On that basis, they neglected inertial effects during collective cell migration. Viscoelastic relaxation is expected to result in long-time-scale stress accumulation and consequently give rise to oscillations through the effective inertia. The stress accumulation can induce local stiffening and on that basis perturb established cell migrated pattern. In general, inertial effects have been discussed in the context of turbulence and quantified by dimensionless Reynolds number $Re = \frac{vL}{\eta}$ (where v is the velocity, L is the characteristic length, ρ is the density, and η is the viscosity). The turbulence of Newtonian liquids is induced at large Re number, i.e., high velocity and low viscosity. However, viscoelastic systems have a few properties that distinguish them from Newtonian fluids [20, 21]. The stress field in viscoelastic systems is not uniquely defined by the current rate of strain, but rather depends on the flow history, with characteristic relaxation times for stress and strain-rate [20]. To the contrary of the turbulence generated within the Newtonian liquids, the so-called “elastic turbulence” appears during flow of viscoelastic liquids such as solutions of flexible long-chain polymers under low Reynolds number $Re \rightarrow 0$, i.e., low velocity and high viscosity [22, 23]. The elastic turbulence represents a consequence of the system viscoelastic nature and is quantified by Weissenberg number $Wi = \frac{v\tau_R}{L}$ (τ_R is the stress relaxation time). For the case of polymer solutions, this elastic turbulence is accompanied by stretching of polymer chains resulting in significant system stiffening. The system stiffening is caused by residual stress accumulation, which leads to sharp growth of the flow resistance. Groisman and Steinberg [23] proposed the dimensionless elastic parameter $X = \frac{Wi}{Re}$ for characterization of the elastic turbulence rather than Re number. Steinberg [24] pointed out that the elastic turbulence of polymer solutions represents the characteristic of large $Wi > 1$ and vanishingly small $Re \ll 1$ number. Larson et al. [25] physically described the elastic parameter X as the ratio between the stress relaxation time τ_R and the viscous diffusion time t_v , i.e., $X = \frac{\tau_R}{t_v}$ (where $t_v = \frac{L^2\rho}{\eta}$). Groisman and Steinberg [26] considered Couette-Taylor (CT) flow of viscoelastic polymer solutions and pointed out that the flow can become unstable when the stress relaxation time is large enough. They considered the oscillatory instabilities generation in highly elastic polymeric

liquids. The rheological response of these systems corresponds to the case when the centrifugal force is totally suppressed by the elastic hoop stress. At those conditions, the flow instabilities in the form of swirls appear as a consequence of this hoop stress. Swirling flow induces inflow and outflow in radial direction driven by action of centrifugal force against elastic force [22]. This important result points out that apparent inertial effects are caused by the system simultaneous stiffening and softening occurring when $R_e \rightarrow 0$ which lead to inflow and outflow. The inflow for $v_r < 0$ (where v_r is the radial velocity component) corresponds to the compression and the outflow for $v_r > 0$ corresponds to extension. Multicellular systems are much complex than polymer solutions, but their viscoelastic nature significantly influences cell rearrangement and should not be neglected [8, 9]. Flow instabilities generated during collective cell migration show similar rheological properties as ones recognized for other viscoelastic systems. However, cellular systems have not been considered in the context of the elastic turbulence yet. Murray et al. [15], Serra-Picamal et al. [2], Tambe et al. [1], and Notbohm et al. [3] neglected inertial effects during collective migration of cell monolayers. This assumption has been supported by low R_e number flow. However, apparent inertial effects could represent a consequence of inflow during cell swirling motion and backward flow during monolayer expansion caused by residual stress accumulation. The aim of this work is to relate viscoelastic nature of cell monolayer during collective cell migration with generated standing and propagative mechanical waves. Consequently, it is necessary to (1) postulate viscoelastic constitutive model for cell monolayer and extracellular matrix; (2) describe cell packing density change, matrix density change, and their interrelation (needed for the description of volume force balance); and (3) formulate the volume force balance that drives cell rearrangement by accounting for two time scales, i.e., a time scale of minutes (for the stress relaxation) and time scale of hours (for collective cell migration, strain change, and residual stress accumulation).

VISCOELASTICITY OF CELL MONOLAYER CAUSED BY COLLECTIVE CELL MIGRATION: THE DIMENSIONLESS CRITERIA

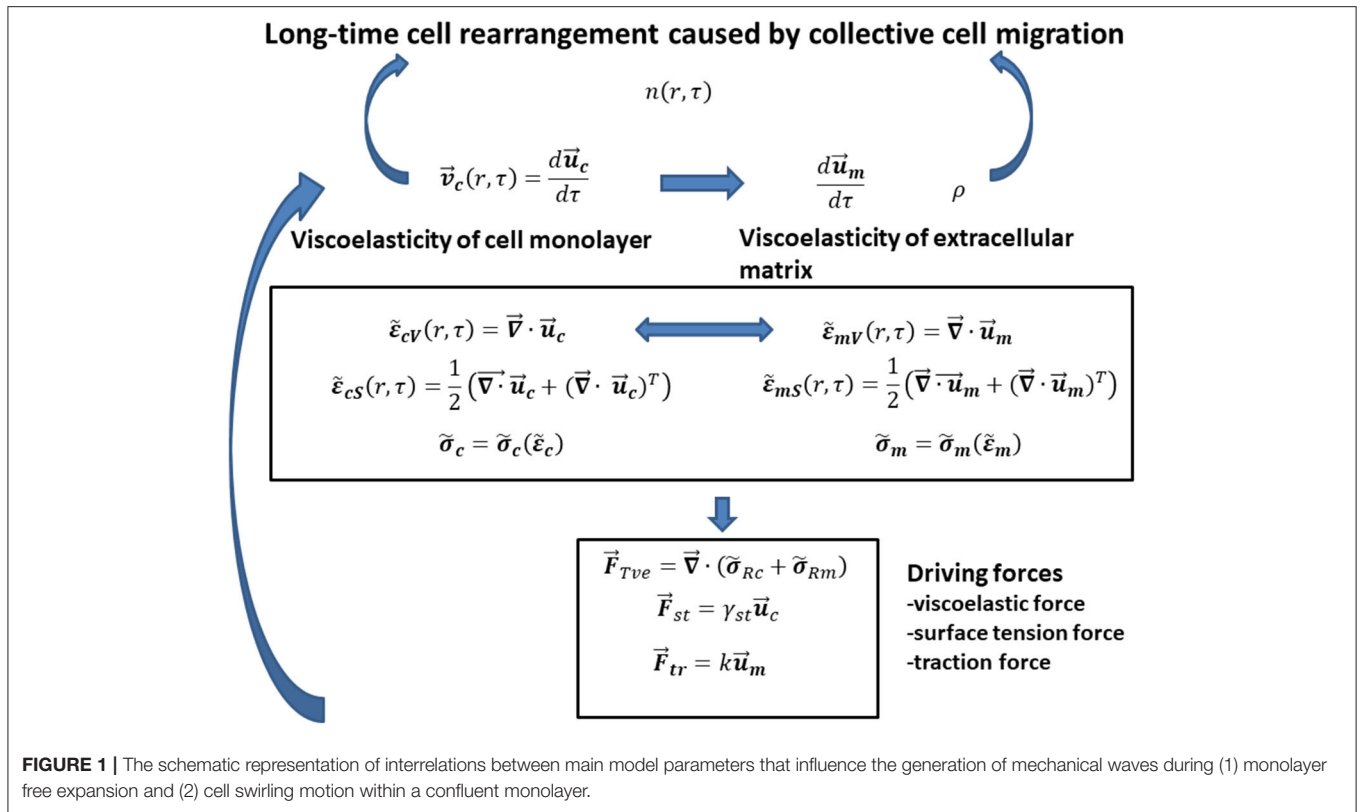
Flow of viscoelastic systems should be characterized by two dimensionless numbers: (1) Reynolds number R_e and Weissenberg number W_i as well as (2) their ratio X [23]. The oscillatory instabilities in the flow, the so-called elastic turbulence, represent the characteristic of large $W_i > 1$ and vanishingly small $R_e \rightarrow 0$ number [24]. The underlying mechanism of this oscillatory phenomenon is related to the coupling of the collective cell migration with the viscoelastic force, which resists the movement. The viscoelastic force arises as a consequence of the residual stress accumulation. While stress relaxation time corresponds to a time scale of minutes, the residual stress accumulation corresponds to a time scale of hours [8, 9, 27]. The parameters R_e and W_i can be estimated based on experimental data from the literature such as (1) the cell velocity

$v_x \sim 0.5 \frac{\mu m}{min}$ [2]; (2) the characteristic length $L = v_x \Delta \tau$ (where $\Delta \tau$ is the period of oscillation equal to $\Delta \tau \approx 4 - 6 h$, [2]); (3) the density of cells could be close to the density of water, i.e., $\rho \sim 1 \frac{g}{cm^3}$; (4) the viscosity of epithelium $\eta = 4.4 \times 10^5 Pa s$ [27]; (5) the stress relaxation time $\tau_R = 3 - 14 min$ [24]; and (6) the characteristic time of residual stress accumulation corresponds to the period of mechanical oscillations $\Delta \tau$ [2, 3]. Instead of W_i , we formulated the effective value of the Weissenberg number, which accounts for the characteristic time for the residual stress accumulation equal to $W_{i,eff} = W_i \frac{\Delta \tau}{\tau_R}$. Corresponding dimensionless numbers are $R_e \sim 10^{-15}$, $W_{i,eff} \sim 0.3$, while $X \sim 10^{14}$. Groisman and Steinberg [23] distinguished critical experimental conditions for the appearance of oscillatory instabilities during flow of polyacrylamide in viscous sugar syrup as a consequence of stress relaxation. They pointed out that critical parameters are $R_e = 0.3$ and $W_i = 3.5$. Generation of oscillatory instabilities in 2D collective cell migration has been experimentally confirmed [2, 3]. For deeply understanding of this complex phenomenon, it is necessary to consider the viscoelasticity of multicellular systems.

CELL LONG-TIME REARRANGEMENT DURING COLLECTIVE CELL MIGRATION: MODELING CONSIDERATION

Cell long-time rearrangement caused by collective cell migration should be discussed based on formulated interrelations between various variables such as (1) cell velocity \vec{v}_c as a function of matrix viscoelasticity $\vec{\sigma}_m = \vec{\sigma}_m(\vec{\epsilon}_m)$, cell viscoelasticity $\vec{\sigma}_c = \vec{\sigma}_c(\vec{\epsilon}_c)$, and cell surface tension γ_{st} and (2) cell packing density n as a function of cell velocity, matrix density ρ , and matrix viscoelasticity (where $\vec{\sigma}_c$ is the cell stress, $\vec{\epsilon}_c$ is the cell strain, $\vec{\sigma}_m$ is the matrix stress, and $\vec{\epsilon}_m$ is the matrix strain). The interrelations between various variables are shown in **Figure 1**.

Consequently, the modeling consideration accounts for the following steps: (1) the expression of cell velocity \vec{v}_c as the rate of change the cell displacement field, i.e., $\frac{d\vec{u}_c}{dt}$ (where \vec{u}_c is the cell displacement field) [8, 9]; (2) the formulation of local cell shear and volumetric strains $\vec{\epsilon}_{cS}$ and $\vec{\epsilon}_{cV}$, respectively, as a function of the cell displacement field [8, 9]; (3) the introduction of a constitutive viscoelastic model for cells $\vec{\sigma}_c = \vec{\sigma}_c(\vec{\epsilon}_c)$ (where $\vec{\sigma}_c$ is the cell stress and $\vec{\epsilon}_c$ is the cell strain) [28, 29]; (4) the formulation of the rate of change the matrix displacement field $\frac{d\vec{u}_m}{dt}$ as a function of $\frac{d\vec{u}_c}{dt}$ [29, 30]; (5) the formulation of local matrix shear and volumetric strains $\vec{\epsilon}_{mS}$, $\vec{\epsilon}_{mV}$, respectively, as a function of the matrix displacement field [29, 30]; (6) the discussion of the rheological behaviors of various matrix applied as a substrate for 2D collective cell migration $\vec{\sigma}_m = \vec{\sigma}_m(\vec{\epsilon}_m)$ (where $\vec{\sigma}_m$ is the matrix stress and $\vec{\epsilon}_m$ is the matrix strain) [2, 3, 30]; (7) the formulation of changing the cell packing density $n(r, \tau)$ as function of various fluxes, such as cell convective flux, conductive flux, durotaxis flux, haptotaxis flux, and galvanotaxis flux [15]; (8) the expression of matrix density change $\frac{\partial \rho}{\partial \tau}$ as a function of matrix convective flux [15]; (9) the formulation of forces that influences cell long-time rearrangement such



as the viscoelastic force, the traction force, and the surface tension force based on modified model proposed by Murray et al. [15]; and (10) the formulation of the interrelation between the cell velocity \vec{v}_c and the forces that influences generation of propagative waves and standing wave based on the corresponding momentum balance. Discussion of cell long-time rearrangement in the context of the elastic turbulence proposed by Groisman and Steinberg [23] is the main goal of this paper.

Viscoelasticity of Multicellular Systems

Viscoelasticity of multicellular systems caused by collective cell migration has been considered on two time scales [8, 9]. The stress relaxation happens at a short-time scale t , whereas the long time scale τ is important for tracking the strain change and the residual stress accumulation as shown in **Figures 2A,B** for (A), a monolayer free expansion inspired by Serra-Picamal et al. [2], and (B), swirling motion of a confluent monolayer inspired by Notbohm et al. [3].

Stress relaxation is primarily induced by adaptation of adhesion contacts and cell shapes [16, 31], which occur at time scale of minutes. However, the local change of strain caused by collective cell migration is slower and occurs at time scale of hours. This long time scale corresponds to collective cell migration, which accounts for cumulative effects of various biochemical processes such as cell signaling and gene expression [6, 32].

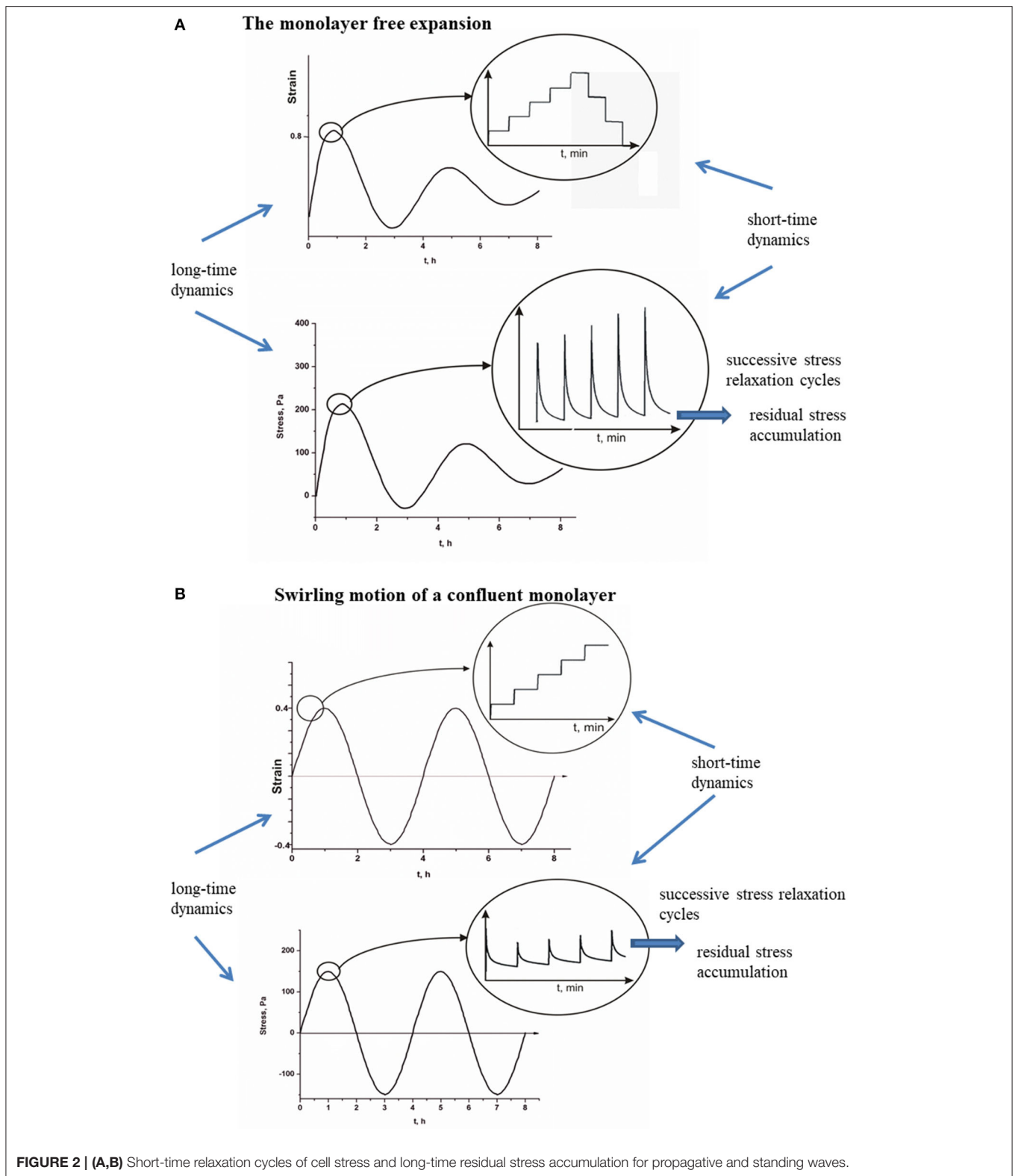
Cell velocity \vec{v}_c can be expressed as follows:

$$\vec{v}_c(r, \tau) = \frac{d\vec{u}_c}{d\tau} \tag{1}$$

where \vec{u}_c is the cell displacement field. The cell local velocity is influenced by various forces such as the viscoelastic force, the traction force, and the surface tension force. Detailed description of the forces and formulation of the force balance is necessary for understanding the mechanical waves. Corresponding cell local volumetric and shear strains depend on \vec{u}_c and can be expressed as follows [8, 9]:

$$\begin{aligned} \tilde{\epsilon}_{cV}(r, \tau) &= (\vec{\nabla} \cdot \vec{u}_c) \tilde{I} \\ \tilde{\epsilon}_{cS}(r, \tau) &= \frac{1}{2} (\vec{\nabla} \vec{u}_c + (\vec{\nabla} \vec{u}_c)^T) \end{aligned} \tag{2}$$

where \tilde{I} is the identity tensor, $\tilde{\epsilon}_{cV}(r, \tau)$ is the cell volumetric strain, and $\tilde{\epsilon}_{cS}(r, \tau)$ is the cell shear strain. Strains induce generation of stress within a cell monolayer. Collective cell migration induces inhomogeneous distribution of stress [9]. Tambe et al. [1] considered long-time residual stress distribution within collective migrated epithelial cell monolayers. Consequently, stress relaxation phenomena have not been reconstructed from their data. Maximum stress accumulation corresponds to 100–150 Pa [1]. However, Marmottant et al. [27] considered stress relaxation of cellular aggregate under constant strain (i.e., the aggregate shape) condition caused by



the aggregate uniaxial compression between parallel plates. The stress decreases exponentially with the relaxation time equal to 3–14 min up to equilibrium value. Stress relaxes from ~ 27 Pa to

the residual stress value equal to ~ 17 Pa during 25 min [27]. This time period corresponds to a short-time cycle. On the other hand, the strain is constant during the short-time cycle and changes

from one stress cycle to another. Maximum average strain rate in x -direction during monolayer free expansion is $\dot{\epsilon}_{xx} \approx 0.29 \text{ h}^{-1}$ [2], while the corresponding period of oscillation is 4–6 h [2, 3].

Stress relaxation ability under constant strain condition represents the characteristic of the viscoelastic solid rather than viscoelastic liquid. The Maxwell model suitable for viscoelastic liquid describes stress relaxation under constant strain rate [20]. However, in the case we considered, the strain change was much slower than the stress relaxation [8, 9]. Accordingly, stress relaxes under constant strain per short-time cycle. Cell stress at a supracellular level accounts for cumulative effects of cell–cell and cell–matrix interactions [17, 33]. Cell–cell interactions influence generation of active forces as a product of the contractility of actomyosin cytoskeleton and cell’s protrusions in the polarization direction. Passive forces accounts for deformation of cells during their migration. Cumulative effects of cell–cell and cell–matrix frictions influence energy dissipation obtained at a long time scale. The cell stress accounts for normal stress and shear stress contributions [9]. Normal and shear stresses consist of elastic and viscous parts and can be expressed as follows: $\tilde{\sigma}_{cV} = \tilde{\sigma}_{cVe} + \tilde{\sigma}_{cVvis}$ for volumetric stress and $\tilde{\sigma}_{cS} = \tilde{\sigma}_{cSe} + \tilde{\sigma}_{cSvis}$ for shear stress (where $\tilde{\sigma}_{cVe}$ and $\tilde{\sigma}_{cSe}$ are elastic contributions, while $\tilde{\sigma}_{cVvis}$ and $\tilde{\sigma}_{cSvis}$ are viscous contributions, respectively), similarly as was formulated by Murray et al. [15] for viscoelastic systems. The simplest constitutive model for a viscoelastic solid capable to describe stress relaxation is the Zener model [28]. The Zener model is expressed as follows:

$$\tilde{\sigma}_c + \tau_R \dot{\tilde{\sigma}}_c = G_c \tilde{\epsilon}_c + \eta \dot{\tilde{\epsilon}}_c \quad (3)$$

where $\dot{\tilde{\sigma}}_c = \frac{d\tilde{\sigma}_c}{dt}$, $\dot{\tilde{\epsilon}}_c = \frac{d\tilde{\epsilon}_c}{dt}$, G_c is the elastic modulus, and η is the viscosity. The relaxation of stress under constant strain condition $\tilde{\epsilon}_{c0}(r, \tau)$ is as follows:

$$\tilde{\sigma}_c(r, t, \tau) = \tilde{\sigma}_{c0} e^{-\frac{t}{\tau_R}} + \tilde{\sigma}_{cR}(r, \tau) \left(1 - e^{-\frac{t}{\tau_R}}\right) \quad (4)$$

where t is the short-time scale, τ is the long time scale, $\tilde{\sigma}_{c0}(\tau)$ is the initial value of the stress for single short-time relaxation cycle, and the stress relaxation time is $\tau_R = \frac{\eta}{G_c}$. The residual stress $\tilde{\sigma}_{cR}(r, \tau)$ is equal to

$$\tilde{\sigma}_{cR}(r, \tau) = G_c \tilde{\epsilon}_{c0}(r, \tau) \quad (5)$$

Notbohm et al. [3] considered 2D cell swirling motion within a confluent monolayer by monitoring long-time change of stress radial component σ_{cRR} . They pointed out that the long-time change of residual stress $\frac{d\sigma_{cRR}}{dt}$ correlated well with the long-time strain change $\frac{d\epsilon_{cRR}}{dt}$ during the time period of 24 h. This result indicates that the Zener model could be suitable for describing the viscoelasticity of cell monolayers because it accounts for experimentally obtained correlations between $\frac{d\sigma_{cRR}}{dt}$ and $\frac{d\epsilon_{cRR}}{dt}$ and describes the stress relaxation. The residual stress accumulation represents the consequence of generated strain and its long-time change [9, 34]. This cause–consequence relation is expressed by the constitutive model (Equations 1–5). The residual stress accumulation induces local stiffening of the monolayer, which

is responsible for generation of flow instabilities. Pajic-Lijakovic and Milivojevic [8, 9, 34] pointed out that the residual stress accumulation can suppress cell migration by decreasing cell velocity and local strain. On that basis, this stress accumulation is a main cause of the generation of apparent inertial effects, which results in the elastic turbulence. For deeper insight into the influence of cell viscoelasticity on the cell velocity in the form of apparent inertial effects, it is necessary to formulate a force balance for (1) monolayer free expansion and (2) cell swirling motion within a confluent monolayer. Besides the viscoelasticity of cells, the viscoelasticity of a supracellular matrix significantly influences cell long-time rearrangement in the context of durotaxes, haptotaxis, and galvanotaxis [15].

Viscoelasticity of an Extracellular Matrix

Various hydrogel matrices have been used as a substrate for cell migration. The rheological behavior of hydrogels frequently corresponds to a poroviscoelasticity [35]. The matrix stress relaxation phenomena caused by cell tractions include (1) the hydrogel viscoelastic relaxation and (2) poroelastic relaxation caused by solvent diffusion. Polyacrylamide gel coated by collagen has been a widely used matrix for 2D cellular systems [1–3]. Hydrogels of natural origins are basement membrane–based gel preparations; some examples include fibrin gel, collagen gel, alginate gel, chitosan gel, and Matrigel [15, 30, 35, 36]. Matrigel is a commercially available basement membrane based gel. These cell–matrix systems are suitable for considering collective cell migration in 2D and 3D. Chaudhuri et al. [37] considered the influence of Ca-alginate viscoelasticity on cell spreading. Chaudhuri et al. [37] and Pajic-Lijakovic et al. [30] proposed the Burgers model for describing the viscoelasticity of Ca-alginate hydrogel. Various hydrogel matrices have been treated as elastic [1–3], while the others have been treated as a viscoelastic [26, 36]. Murray et al. [15] proposed the Kelvin-Voigt model for describing the viscoelasticity of fibrous extracellular matrices. Pajic-Lijakovic et al. [29] described the long-time change of the matrix displacement field $\frac{d\vec{u}_m}{dt}$ by cell action as follows:

$$\frac{d\vec{u}_m(r, \tau)}{d\tau} = \frac{\delta F_m}{\delta \vec{u}_m} + \frac{d\vec{u}_c(r, \tau)}{d\tau} \quad (6)$$

where F_m is the free energy function that accounts for cell–matrix mechanical and electrostatic interactions, and $\vec{u}_c(r, \tau)$ is the cell displacement field. The first term of the right-hand side of Equation (6) accounts for the rheological response of a matrix caused by its structural changes, whereas the second one represents the driving force for the matrix displacement field fluctuations. The corresponding matrix volumetric and shear strains are equal to

$$\begin{aligned} \tilde{\epsilon}_{mV}(r, \tau) &= (\vec{\nabla} \cdot \vec{u}_m) \tilde{\mathbf{I}} \\ \tilde{\epsilon}_{mS}(r, \tau) &= \frac{1}{2} \left(\vec{\nabla} \vec{u}_m + (\vec{\nabla} \vec{u}_m)^T \right) \end{aligned} \quad (7)$$

where $\tilde{\epsilon}_{mV}(r, \tau)$ is the matrix volumetric strain and $\tilde{\epsilon}_{mS}(r, \tau)$ is the matrix shear strain. Corresponding matrix stress-strain constitutive model $\tilde{\sigma}_m = \tilde{\sigma}_m(\tilde{\epsilon}_m)$ depends on the choice of the

matrix and the type of cells (where $\tilde{\sigma}_m$ is the matrix stress). Cell traction force depends on the matrix displacement field and was expressed as $\vec{F}_{tr} = k\vec{u}_m$ (where k is an elastic constant) [15]. Pajic-Lijakovic et al. [30] considered residual stress accumulation $\tilde{\sigma}_{Rm}$ within Ca-alginate hydrogel matrix without cells. It is useful in order to estimate cell–matrix interactions. They pointed out that the increase in the residual stress within the Ca-alginate matrix was significant (~ 7 kPa) after 10 repeated cycles, even under a low externally induced compression strain of 2% per cycle.

Cell migration speed, cell packing density, and correlation of cell migration depend on cell–matrix mechanical and electrostatic interactions, which influence the state of cell–matrix adhesion contacts and on that basis the state of single cells. Viscoelasticity of matrix influences accumulated stress within a monolayer and on that basis the correlation of cell migration [38]. Intensive cell stress accumulation can perturb and even suppress cell migration. This cause–consequence relation was to be discussed based on (1) the rate of change the cell packing density [15] and (2) the force balance formulated by modified the model proposed by Murray et al. [15]. The cell speed has been correlated with the matrix stiffness. The speed of migrating cells is lower at softer matrices due to weak traction and cell slipping [39]. However, high matrix stiffness leads to a decrease in the migration speed caused by cell–matrix adhesion strengthening. Thus, medium matrix stiffness is suitable for cell migration. The relation between matrix stiffness and cell spreading can be expressed in the form of durotaxis flux \vec{J}_d [15] as follows:

$$\vec{J}_d = k_d n \vec{\nabla} G_{sm} \quad (8)$$

where k_d represents a measure of cell–matrix mechanical interactions, which influence the matrix displacement field \vec{u}_m and the state of cell–matrix adhesion contacts, $n(r, \tau)$ is the packing density of cells, and G_{sm} is the elastic shear modulus of a matrix. Besides of the matrix viscoelasticity, the matrix density is also influenced by cell–matrix interaction. Long-time change of the matrix density has the feedback impact on the packing density of cells as well. The phenomenon can be expressed in the form of haptotaxis flux [15] as follows:

$$\vec{J}_h = k_h n \vec{\nabla} \rho \quad (9)$$

where k_h is the measure of cell–matrix interactions which influences the matrix density ρ . Change of the matrix density ρ caused by cell tractions has been described by Murray et al. [15] in the form of matrix convective flux as:

$$\frac{\partial \rho}{\partial \tau} = -\vec{\nabla} \cdot \left(\rho \frac{d\vec{u}_m}{d\tau} \right) \quad (10)$$

where $\frac{d\vec{u}_m}{d\tau}$ is the matrix displacement field change expressed by Equation (6). Cell tractions induce water outflow from the hydrogel by changing its density as well as the rheological behavior. Polyelectrolyte nature of matrix influences cell–matrix electrostatic interactions as well as the state of cell–matrix

adhesion contacts. The good example is Ca-alginate hydrogel matrix [30]. Electrostatic interchain and intrachain interactions caused by cell tractions influence the residual stress accumulation within a matrix $\tilde{\sigma}_{mR}$, which has the feedback impact to the matrix local stiffness. The phenomenon can be expressed in the form of galvanotaxis flux [15] as follows:

$$\vec{J}_g = k_g n \vec{\nabla} \phi_e \quad (11)$$

where k_g is the measure of cell–matrix electrostatic interactions, and ϕ_e is the local electrostatic potential.

Long-Time Change of Cell Packing Density

Cell packing density change $\frac{\partial n(r, \tau)}{\partial \tau}$ is a product of cell–cell and cell–matrix interactions. It is self-regulated property due to the contact inhibition during collective cell migration and force-induced cell repolarization [17, 39]. Several processes have been accounted for such behaviors as follows: (1) contact inhibition of locomotion (CIL), (2) contact following of locomotion, and (3) contact enhancement of locomotion [17]. Cell packing density change during collective cell migration is expressed as follows [15]:

$$\frac{\partial n(r, \tau)}{\partial \tau} = -\vec{\nabla} \cdot \vec{J} \quad (12)$$

where \vec{J} is the flux of cells equal to $\vec{J} = \vec{J}_{conv} + \vec{J}_{cond} + \sum_i \vec{J}_i$, such that $\vec{J}_{conv} = n \vec{v}_c$ is the convective flux, \vec{v}_c is cell velocity (Equation 1), $\vec{J}_{cond} = -D_{eff} \vec{\nabla} n$ is the conductive flux, D_{eff} is the effective diffusion coefficient, and $\vec{J}_i = k_i n \vec{\nabla} \phi_i$, are haptotaxis, durotaxis, plitotaxis, galvanotaxis, and chemotaxis fluxes such that $\phi \equiv \rho$ is the matrix density for the haptotaxis, $\phi \equiv \phi_e$ is the electrostatic potential for the galvanotaxis, $\phi \equiv c$ is the concentration of nutrients for the chemotaxis, $\phi \equiv G_{sm}$ is the local shear modulus of a matrix for the durotaxis, $\phi \equiv G_{sc}$ is the local shear modulus of cells for plitotaxis, whereas k_i is the model parameter that accounts for various types of interactions such as mechanical, electrostatic, or chemical. Conductive flux accounts for cell response to a local variation of cell density. Haptotaxis, durotaxis, and galvanotaxis fluxes account for cell–matrix mechanical and electrostatic interactions. The tractions exerted by cells on the matrix generate gradients in (1) the matrix density and correspondingly the haptotaxis flux, (2) the electrostatic potential and the galvanotaxis flux, and (3) the matrix stiffness and the durotaxis flux [15]. Chemotaxis flux accounts for cell response to a concentration of nutrients [15]. Plitotaxis flux represents the consequence of cell–cell mechanical interactions, which leads to the establishing of gradients in cell shear modulus. Cell mitosis is neglected at this time scale. Rieu et al. [40] reported that diffusion coefficient for collectively migrated endodermal cells is $D_{eff} = 0.45 \pm 0.2 \frac{\mu m^2}{min}$, whereas for ectodermal cells the diffusion coefficient is $D_{eff} = 1.05 \pm 0.4 \frac{\mu m^2}{min}$. If the conductive mechanism is dominant, the model Equation (12) becomes the second Fick's law. In this case, the solution for the density is oscillatory in space. If the convective mechanism is dominant, the oscillatory change of the cell packing density

can be induced only by oscillatory change of the cell velocity. At this step of consideration, it is necessary to determine which mechanism is dominant convective or conductive during 2D cell migration. To do so, we postulated following condition:

1. if $L_{\max} \leq \sqrt{t_C D_{\text{eff}}}$, the conductive mechanism is dominant, and
2. if $L_{\max} \gg \sqrt{t_C D_{\text{eff}}}$, the convective mechanism is dominant.

where t_C is the period of long-time oscillations equal to $t_C \approx 4 - 6 h$ [2, 3], and L_{\max} is the maximum velocity correlation length. As the cell packing density increases and cells become more dense and slow down their movement, the correlation length first increases to ~ 10 -cell lengths or $L_{\max} \sim 150 \mu m$ and later decreases [41, 42]. The result of this simple calculation points out that the convective mechanism dominantly influences the cell packing density change, while the conductive mechanism can be neglected. This finding indicates that oscillatory changes of cell packing density come primarily from the oscillatory change of cell velocity.

Cell long-time rearrangement is described by interrelation between the following variables such as (1) the displacement of cells \vec{u}_c (Equation 1) and corresponding cell volumetric and shear strains, (2) the displacement of matrix \vec{u}_m (Equation 6) and corresponding matrix volumetric and shear strains, (3) the cell packing density n (Equation 12), and (4) the matrix density ρ (Equation 10). Displacement fields of cells and matrix induce generation of strains. The strains lead to generation of the corresponding stresses based on the proposed constitutive models for cells and for a matrix. Oscillatory change of one variable induces oscillatory changes of the others. For deeper understanding of this oscillatory dynamic, it is necessary to formulate the force balance for (1) monolayer expansion and (2) cell swirling motion within a confluent monolayer.

THE FORCE BALANCE

The force balance is responsible for oscillatory patterning the cell long-time rearrangement. Murray et al. [15] formulated the momentum balance by neglecting inertia effects as $\sum_i \vec{F}_i = 0$. They supported this assumption by pointing out the fact that the corresponding R_e number is low. The force balance proposed by Murray et al. [15] should be expanded by accounting for the additional surface tension force \vec{F}_{st} which significantly influences the monolayer free expansion [43]. The surface tension has been recognized as one of the key parameters, which influences cell aggregate rounding after uniaxial compression [27]. The aggregate rounding occurs via collective cell migration [27]. The resulted force balance can be expressed as follows:

$$\sum_i \vec{F}_i = \rho \vec{F}_{tr} - \vec{F}_{Tve} - n \vec{F}_{st} \tag{13}$$

where $\vec{F}_{tr} = k \vec{u}_m$ is the cell traction force, k is an elastic constant [15], $\vec{F}_{st} = \gamma_{st} \vec{u}_c$ is the surface tension force, γ_{st} is the surface tension, \vec{u}_c is the cell displacement field, \vec{F}_{Tve} is the viscoelastic force per unit volume equal to

$\vec{F}_{Tve} = \vec{\nabla} \cdot (\vec{\sigma}_{Rc} - \vec{\sigma}_{Rm})$, $\vec{\sigma}_{Rc}$ is the cell residual stress (Equation 5), and $\vec{\sigma}_{Rm}$ is the matrix residual stress. Consequently, the viscoelastic force accounts for cell and matrix contributions. The \vec{F}_{Tve} is the resistive force directed always opposite to the direction of migration. The surface tension force $n \vec{F}_{st}$ always acts in order to decrease a surface and on that basis to decrease a surface free energy. When cells undergo the forward flow during monolayer expansion, both forces \vec{F}_{Tve} and $n \vec{F}_{st}$ act in the direction opposite of migration in order to resist this movement. However, when cells undergo the backward flow driven by the surface tension force $n \vec{F}_{st}$, the viscoelastic force \vec{F}_{Tve} acts in the direction opposite of backward flow. The traction force $\rho \vec{F}_{tr}$ acts in the direction of cell migration and influences the rate of cell expansion depending on the rheological behavior of a matrix [3, 15, 30]. The force balance is established and perturbed many times during collective cell migration. These perturbations are primarily induced by accumulation of the residual stress within a multicellular system [8, 9] and by cell adaptation under stress conditions [16]. In order to completely understand this complex dynamic of cell long-time rearrangement, it is necessary to distinguish (1) equilibrium regimens for which $\sum_i \vec{F}_i = 0$ and (2) perturbed regimens for which $\sum_i \vec{F}_i \neq 0$ in various experimental conditions. Every perturbation induces change of cell velocity \vec{v}_c and corresponding strain rates $\dot{\vec{e}}_{cV}$ and $\dot{\vec{e}}_{cS}$, and on that basis provokes the cell rheological response, which can lead to a local softening or stiffening of monolayer parts. Local stiffening represents a consequence of the cell residual stress $\vec{\sigma}_{Rc}$ accumulation [9]. Consequently, the momentum balance can be expressed in the form of inertial wave equation:

$$n \frac{D \vec{v}_c}{D \tau} = \rho \vec{F}_{tr} - \vec{F}_{Tve} - n \vec{F}_{st} \tag{14}$$

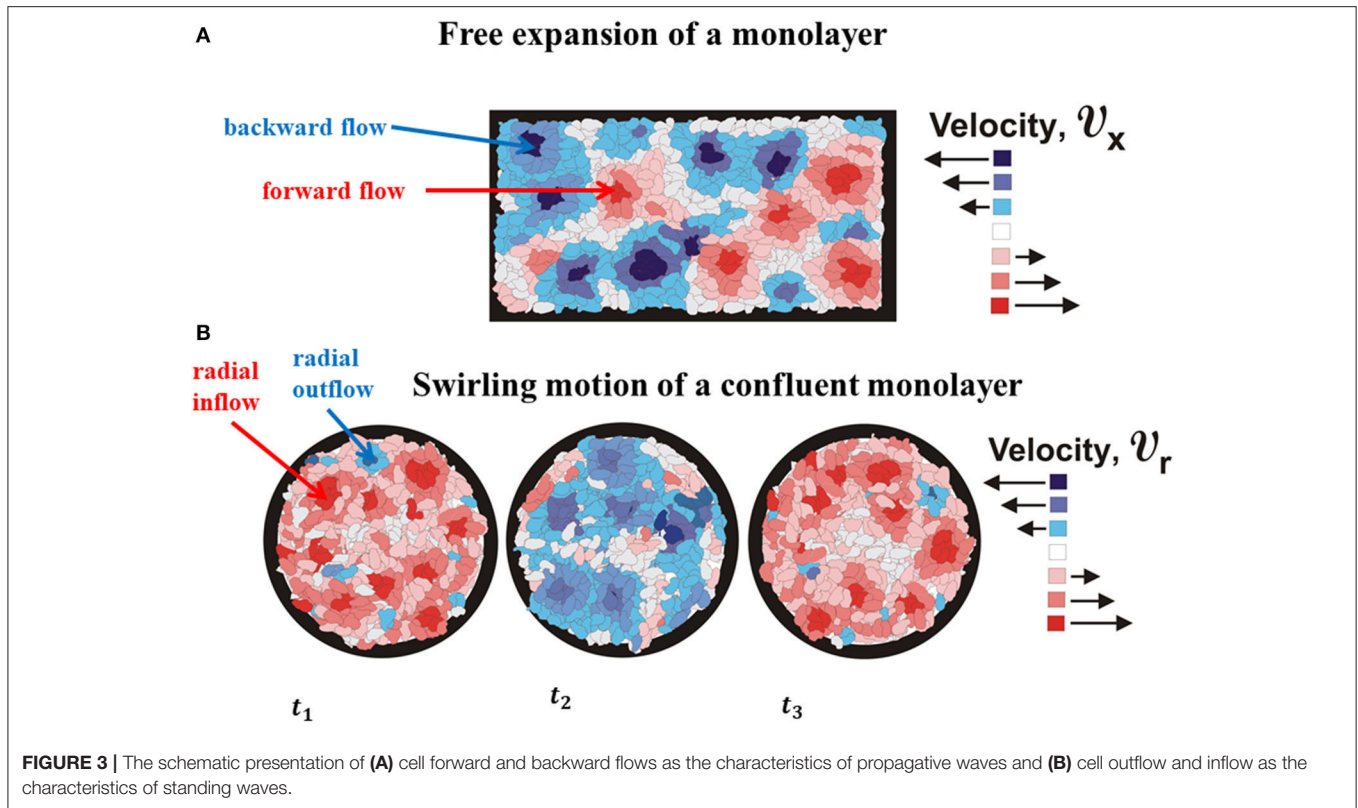
where $\frac{D \vec{v}_c}{D \tau} = \frac{\partial \vec{v}_c}{\partial \tau} + (\vec{v}_c \cdot \vec{\nabla}) \vec{v}_c$ is the material derivative [44]. The left-hand side of Equation (14) corresponds to the resultant force. Inertial waves, i.e., inertial oscillations, are a type of mechanical waves. The perturbations of the force balance, caused by cell viscoelasticity, represent the main cause for generation of (1) propagative waves during monolayer free expansion and (2) standing waves during collective cell migration within a confluent monolayer. Consequently, various types of perturbations were to be elaborated in more details.

Propagative Waves Generation in a Freely Expanded Monolayer: Modeling Consideration

The free expansion of a cell monolayer has been considered in 2D by using Cartesian coordinates such that $\vec{v}_c = \vec{v}_c(v_{cx}, v_{cy})$ (where v_x and v_y are the velocity components) [2]. The corresponding momentum balance can be expressed as follows:

For x -direction:

$$n \left(\frac{\partial v_{cx}}{\partial \tau} + v_x \frac{\partial v_{cx}}{\partial x} + v_y \frac{\partial v_{cx}}{\partial y} \right) = \rho F_{trx} - F_{Tve x} - n F_{stx} \tag{15}$$



For y -direction:

$$n \left(\frac{\partial v_{cy}}{\partial \tau} + v_x \frac{\partial v_{cy}}{\partial x} + v_y \frac{\partial v_{cy}}{\partial y} \right) = \rho F_{tr y} - F_{Tve y} - n F_{st y}$$

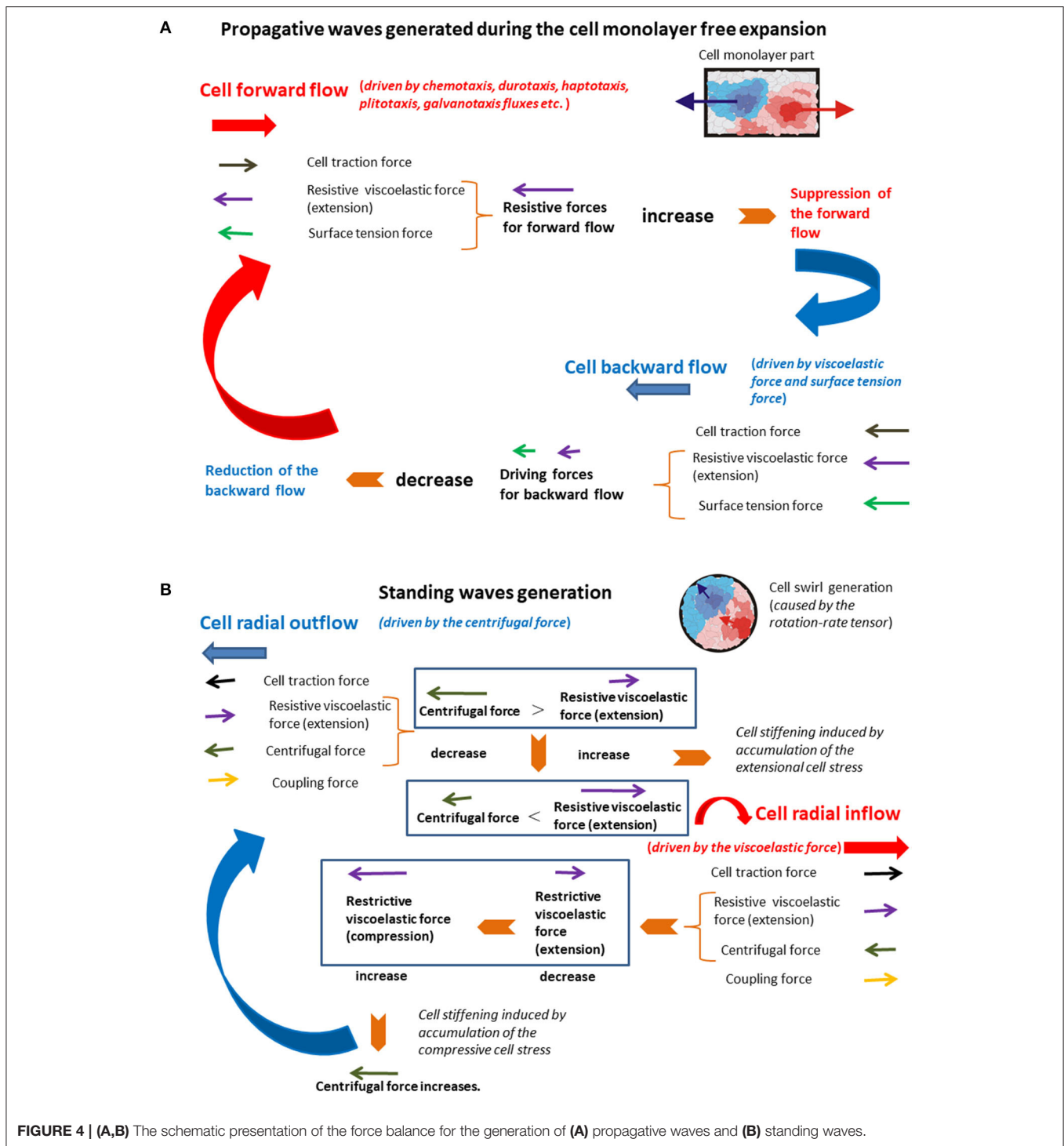
The monolayer expansion occurs in two opposite directions, i.e., $x \in (0, L(\tau))$ and $x \in (0, -L(\tau))$. The main characteristic of propagative waves is that (1) normal stress component σ_{cxx} and corresponding strain rate $\dot{\epsilon}_{cxx}$ are in phase quadrature; (2) normal stress component is always tensional; and (3) velocity and cell tractions are uncorrelated [2, 5]. These periodic extensions of multicellular domains lead to alternate softening and stiffening of cell monolayer. The periodic change of the rheological behavior is connected to the forward flow and backward flow, which is experimentally confirmed by Serra-Picamal et al. [2]. These forward flow and backward flow were shown schematically in Figure 3.

Serra-Picamal et al. [2] considered a free expansion of Madin-Darby canine kidney type II cells on polyacrylamide gels. Cellular domains that undergo forward flow can be divided into two regimens: (1) initial, unlimited cell migration, which corresponds to the condition that cell velocity increases with x , i.e., $\dot{\epsilon}_{cxx} > 0$; and (2) final limited cell migration, which corresponds to the condition that cell velocity decreases with x , i.e., $\dot{\epsilon}_{cxx} < 0$ (where $\dot{\epsilon}_{cxx}$ is the volumetric strain rate in x -direction equal to $\dot{\epsilon}_{cxx} = \frac{\partial v_{cx}}{\partial x}$ and v_{cx} is the x -component of cell velocity) [2]. Maximum velocity for the forward flow is $v_{cx}^{\max} \approx 1 \frac{\mu m}{min}$ [2]. The characteristic of the domains with maximum cell velocity is the intensive normal and shear

residual stresses accumulation up to $\sim 400 Pa$ [2]. Cellular domains that undergo backward flow are unstable primarily due to collisions with surrounding cell domains, which undergo the forward flow. These collisions additionally reduce the cell velocity within surrounding domains under forward flow. The lifetime of domains under backward flow is shorter than the period of oscillations due to (1) domain collisions and (2) rapid decrease in the surface tension force, which drives the backward flow. The phenomenon will be explained in detail in a few steps.

The initial unlimited forward flow of cellular domains leads to their extension. When the extension becomes significant, it induces (1) an increase in the resistive force \vec{F}_{Tve} caused by accumulation of the residual stress, which leads to the monolayer local stiffening; and (2) an increase in the surface tension force $n \vec{F}_{st}$. Both forces act to suppress the cell forward flow (Figure 4A).

This state corresponds to the limited forward flow. Cell domains that correspond to the unlimited forward flow conditions are softer than those related to the limited forward flow conditions due to an accumulation of the cell residual stress. The local stiffening of the monolayer, which corresponds to the limited forward flow regime, is induced by the extension of adhesion contacts and force-induced repolarization (FIR) [17]. When the cell velocity tends to zero $\vec{v}_c \rightarrow 0$ and the surface tension force $n \vec{F}_{st}$ becomes large enough, they induce onset of the backward flow by decreasing the displacement \vec{u}_c (thus reducing the surface tension force $n \vec{F}_{st}$ itself), which leads to



rapid reduction of the backward flow. Collision of backward flow domains with surrounding domains under forward flow additionally suppresses the backward flow. This backward flow leads to the monolayer local softening and decreases in both forces \vec{F}_{Tve} and $n\vec{F}_{st}$, which establishes the unlimited forward flow again. The action of the viscoelastic force to forward flow and backward flow is not symmetric and induce delay

effects. The action of viscoelastic force and the surface tension force in order to suppress the forward flow and generate the backward flow are responsible for periodical extension of the monolayer in the form of propagative waves. Stiffer domains, which correspond to the limited forward flow regimen, form some kind of supracellular network within a monolayer. This supracellular network has a main role in keeping cellular integrity

during the monolayer free expansion. The supracellular network formation is experimentally confirmed by Serra-Picamal et al. [2]. After consideration of the standing waves generation, the comparative analysis of the main characteristics of both types of waves was to be performed from the standpoint of single cells.

Standing Waves Generation in Confluent Cell Monolayers

Collective cell migration within a confluent monolayer leads to cell swirling motion [3]. The prerequisite of cell swirl appearing is the reduction of cell polarity alignment (LA) and strong CIL as reported by Lin et al. [45]. Weak LA and strong CIL can be established under confluent environment. Collective cell migration induces a gradient of velocity field during shear flow. The gradient of the velocity field $\vec{\nabla} \vec{v}_c = \frac{1}{2} (\dot{\tilde{\epsilon}}_{cs} + \dot{\tilde{\omega}}_c)$ can be decomposed into its symmetric and antisymmetric parts [where $\tilde{\epsilon}_{cs}$ is the symmetric shear-rate tensor equal to $\tilde{\epsilon}_{cs} = \frac{1}{2} (\vec{\nabla} \vec{v}_c + (\vec{\nabla} \vec{v}_c)^T)$] and $\dot{\tilde{\omega}}_c$ is the antisymmetric rotation-rate tensor equal to $\dot{\tilde{\omega}}_c = \frac{1}{2} (\vec{\nabla} \vec{v}_c - (\vec{\nabla} \vec{v}_c)^T)$. The tensor $\dot{\tilde{\omega}}_c$ is responsible for the cell swirling motion if the conditions of weak LA and strong CIL are satisfied [45]. Cell swirling motion within a confluent monolayer has been considered in 2D by using cylindrical coordinates, i.e., $\vec{v}_c = \vec{v}_c(v_{cr}, v_{c\theta})$ (where v_{cr} is the radial component and $v_{c\theta}$ is the azimuthal component of velocity) [3]. A circular cell motion induces the generation of internal centrifugal force equal to $F_C = n \frac{v_{c\theta}^2}{r}$ responsible for radial extension of the swirl parts and local radial outflow such that $v_{cr} > 0$. The centrifugal force decreases with an increase in r . Consequently, the action of the centrifugal force is more intensive in the swirl core region in comparison with the peripheral region. The viscoelastic force \vec{F}_{Tve} is the resistive force and acts against centrifugal force in order to suppress cell migration. The traction force $\rho \vec{F}_{tr}$ acts in the direction of cell migration and influences the rate of cell spreading depending on the rheological behavior of a matrix [3, 15, 30]. The surface tension force $n \vec{F}_{st}$ can be neglected during collective cell migration within a confluent monolayer.

The corresponding momentum balance can be expressed as follows:

For r -direction:

$$n \left(\frac{\partial v_{cr}}{\partial \tau} + v_r \frac{\partial v_{cr}}{\partial r} + \frac{v_{c\theta}}{r} \frac{\partial v_{cr}}{\partial \theta} - \frac{v_{c\theta}^2}{r} \right) = \rho F_{tr r} - F_{Tve r} \quad (16)$$

For θ -direction:

$$n \left(\frac{\partial v_{c\theta}}{\partial \tau} + v_{cr} \frac{\partial v_{c\theta}}{\partial r} + \frac{v_{c\theta}}{r} \frac{\partial v_{c\theta}}{\partial \theta} + \frac{v_{cr} v_{c\theta}}{r} \right) = \rho F_{tr \theta} - F_{Tve \theta}$$

where the internal centrifugal is equal to $F_C = n \frac{v_{c\theta}^2}{r}$, and the force that accounts for coupling between radial elongation (or compression) with azimuthal shear flow is expressed as

$F_{CL} = n \frac{v_{cr} v_{c\theta}}{r}$. The coupling force F_{CL} acts to reinforce the radial flow [22].

The standing waves represent a characteristic of local cell rearrangement, which leads to swirling motion. The main characteristics of standing waves are (1) the radial velocity and cell tractions are uncorrelated, (2) normal stress component σ_{crr} and the corresponding strain rate $\dot{\epsilon}_{crr}$ are uncorrelated, (3) normal stress component is simultaneously tensional and compressional, and (4) time derivative of the stress component is in phase with the corresponding strain rate component [3]. Coordinated motion of close-packed cell monolayer with confining border leads to local swirling. Critical diameter of swirls is $\sim 250 \mu m$, above which global rotation is substituted by smaller vortices and transient coordinated flow. This value of the critical diameter is expected if we have in mind that the velocity correlation length is $\sim 150 \mu m$ [5].

Notbohm et al. [3] considered confluent migration of Madin-Darby canine kidney type II cells on polyacrylamide gels. They reported that radial component of velocity v_{cr} simultaneously changes a direction every ~ 4 to 6 h. The velocity v_{cr} is approximately constant within domains $\Delta r \sim 30$ to $40 \mu m$ during the time period $\Delta \tau \sim 1$ to 2 h and fluctuates in the same direction within a time period of ~ 4 to 6 h [3]. The corresponding local strain rate is $\dot{\epsilon}_{crr} \approx 0$ during the time period $\Delta \tau \sim 1$ to 2 h. If the $\dot{\epsilon}_{crr} \approx 0$, it means that the corresponding strain component is $\epsilon_{crr} \approx const$. The maximum radial velocity is equal to $v_{cr}^{max} \approx 0.25 \frac{\mu m}{min}$, while the maximum normal residual stress is $\sim 300 Pa$ for extension and $\sim -300 Pa$ for compression. The swirling motion of the viscoelastic multicellular system induces generation of the standing waves. This type of waves will be considered in the context of cell inflow and outflow within a swirl (Figure 3). Presence of inflow and outflow during a cell swirling motion is recognized experimentally by Notbohm et al. [3]. These inflow and outflow are shown schematically in Figure 4B.

Radial extension of swirl parts (the cell outflow for $v_{cr} > 0$ and $\frac{\partial v_{cr}}{\partial \tau} \approx 0$ during $\Delta \tau$, [3]) caused by the action of the centrifugal force induces intensive coupling between radial elongation flow and azimuthal shear flow and an increase in the viscoelastic force \vec{F}_{Tve} , which leads to the local system stiffening. The system stiffening leads to a decrease in the cell velocity component $v_{c\theta}$, as well as a decrease in the centrifugal force, which causes the cell radial inflow and consequently the local compression of swirl parts. The inflow is characterized by the radial component of velocity such that $v_{cr} < 0$ and $\frac{\partial v_{cr}}{\partial \tau} \approx 0$ during $\Delta \tau$ [3]. The inflow induces change of the viscoelastic force direction from extension to compression, which results in the increase in the centrifugal force. Consequently, the viscoelastic (elongation) force resists the outflow, while the viscoelastic (compressive) force resists the inflow. The increase in the centrifugal force leads to the system outflow again characterized by the radial component of velocity $v_{cr} > 0$. The centrifugal force is larger in the swirl core region in comparison with the peripheral region. Consequently, the inflow and outflow events are more intensive in the core region as was experimentally observed by Notbohm et al. [3]. The action of the viscoelastic force to the inflow and outflow is not symmetric

and induces delay effects [22]. These delay effects can induce time shift between inflow and outflow. This time shift induces perturbations of inflow–outflow dynamic, which leads to altered extension and compression of the swirl parts. These long-time cycles correspond to standing waves. Differences between these two types of mechanical waves were to be discussed from the standpoint of single cells.

RESULTS AND DISCUSSION

The aim of this theoretical consideration is to emphasize the role of viscoelasticity in provoking apparent inertial effects and generating the oscillatory mechanical instabilities in the form of standing waves and propagative waves within multicellular systems caused by collective cell migration. The propagative waves are generated during monolayer expansion, while the standing waves are generated during the cell swirling motion within a confluent monolayer. These flow instabilities represent a characteristic of the elastic turbulence that occurs under low Re number. The phenomenon has been experimentally confirmed during flow of various viscoelastic systems such as polymer liquids [23, 25], and it has been recognized in experiments of 2D collective cell migration but has not been explained properly yet [1–3]. The elastic turbulence is induced primarily by viscoelastic force, which acts against a movement of the system constituents. The system viscoelastic response under migration is a product of the energy storage and energy dissipation caused by its structural ordering. The structural ordering accounts for orientation and deformation of the system constituents in the direction of flow, which can induce significant accumulation of residual stress and the system stiffening. The system stiffening changes the characteristic of flow, which has the feedback impact to its rheological behavior. This cause–consequence cycle can be understood in the form of apparent inertial effects, which leads to generation of mechanical waves [22].

Multicellular systems are much complex than polymer liquids, but their viscoelastic nature significantly influences characteristics of collective cell migration [8, 9]. In this case, the system structural ordering accounts for cumulative effects of various interrelated processes at cellular and supracellular levels. Processes at cellular level are cell activation, polarization, signaling, and changes the state of cell–cell and cell–matrix adhesion contacts [16, 20, 32, 46]. Processes at the supracellular level account for cumulative effects of processes at the cellular level. These are polarity alignment, polarity–flow alignment, contact regulation of locomotion, and FIR [17, 33, 47].

Generation of mechanical waves caused by collective cell migration accounts for cause–consequence relations between (1) cell packing density $n(r, \tau)$ change (Equation 12) as the result of cell–cell and cell–matrix interactions described by convective, conductive, haptotaxis, durotaxis, galvanotaxis, plitotaxis, and chemotaxis fluxes; (2) matrix density $\rho(r, \tau)$ change (Equation 10) as the result of cell–matrix interactions described by convective flux caused by cell tractions; (3) force balance equation (Equation 14), which relates cell velocity with viscoelasticity

of multicellular system; viscoelasticity of a matrix; cell surface tension; cell tractions; cell packing density; and matrix density.

A long-time cell rearrangement during monolayer expansion is accomplished by local forward flow and backward flow. The forward flow is divided into two regimens unlimited forward flow and limited forward flow. The limitations come from the action of the viscoelastic force against migration. The forward flow induces an accumulation of the extensional residual stress and an increase in the resistive viscoelastic force, which leads to the stiffening of monolayer parts and suppresses cell migration. The forward flow also induces an increase in cell displacement field and on that basis an increase in the surface tension force. Once the forward flow is suppressed, the surface tension force induces the backward flow, which leads to (1) a decrease in the surface tension force itself and (2) the softening of the monolayer part. The backward flow decreases rapidly because of (1) a decrease in the surface tension force and (2) collisions with surrounding domains under forward flow. This softening results in a decrease in the viscoelastic force. Lower values of the viscoelastic force as well as the surface tension force induce forward flow of the monolayer again. Those long-time cycles repeat many times in the form of the propagative waves [2].

A long-time cell rearrangement during the cell swirling motion (within a confluent monolayer) should be considered in the context of cell radial inflow and outflow. The confluence induces reduction of cell polarity alignment, which is essential for appearing cell swirls [45]. The inflow and outflow are induced by action of the centrifugal force against the viscoelastic force. The centrifugal force leads to radial extension of swirl parts, which results in the cell outflow. This radial extension causes an increase in the viscoelastic force, which leads to the system local stiffening. The viscoelastic force suppresses cell migration by increasing the residual stress accumulation, which results in a decrease in the centrifugal force. The consequence of the centrifugal force decrease is the radial cell inflow, which leads to the softening of swirl parts. This softening causes a decrease in the viscoelastic force and consequently the increase in the centrifugal force responsible for the cell outflow again. Those long-time cycles repeat many times in the form of the standing waves [3].

Both types of waves represent a consequence of apparent inertial effects. The apparent inertial effects are related to the periodic generation of (1) the backward flow during monolayer expansion and (2) the inflow during a cell swirling motion. The maximum velocity for (1) inflow and outflow is $\sim 0.25 \frac{\mu m}{min}$, and (2) forward flow and backward flow is $\sim 1 \frac{\mu m}{min}$. The maximum extensional stress accumulated during (1) forward flow is $\sim 300 Pa$ and (2) outflow is $\sim 400 Pa$. It would be interesting to calculate maximum extensional stress necessary to break cell–cell adherens junction (AJs). AJs are cadherin–catenin complexes linked to actin filaments. Cadherins are transmembrane glycoproteins containing an extracellular domain that mediates cell–cell adhesion via homophilic or heterophilic interactions and an intracellular domain that controls signaling cascades involved in a variety of cellular processes, including polarity, gene expression, etc. [7]. E-cadherin bond breakage requires the force of $\sim 200 nN$, while the

maximum area of single AJ is $\sim 100 \mu\text{m}^2$ [48]. It corresponds to the extensional stress equal to $\sim 2 \text{kPa}$. This result means that forward flow and backward flow and inflow and outflow are not capable to perturb the integrity of multicellular system.

The main difference between propagative waves generated during monolayer expansion and standing waves generated during cell swirling motion within a confluent monolayer is related to oscillatory stress change. Generated propagative waves induce damped oscillatory change of the extensional residual stress, whereas the compressive stress is not generated based on the experimental data by Serra-Picamal et al. [2] (**Figure 2A**). To the contrary with the propagative waves, the generation of standing waves induces altered extension and compression [3] (**Figure 2B**). Corresponding stress oscillations were not damped during time period of 24 h. This difference can be discussed in the context of two cellular processes: (1) contact regulation of locomotion (CRL) and (2) FIR. The CRL depends strongly on the cell–cell collision angle [15, 36]. While the forward flow and backward flow act parallel to the direction of migration, the inflow and outflow act perpendicular to the direction of migration. The forward flow and backward flow intensify cell head-to-tail interactions and induce periodic cell repolarization in the direction of flow by keeping the strong of AJs [39]. Reinforced AJs are capable to resist strain and reduce residual stress accumulation [49]. Consequently, the backward flow induces a decrease in the extensional stress rather than to create cell compression. The inflow and outflow intensify cell side-to-side interactions, which can induce cell depolarization and weakening of AJs [16]. Consequently, the inflow can lead to the accumulation of compressive residual stress.

Model developed can be applied to describe generation of mechanical waves within 3D multicellular systems. Standing waves as a characteristic of the cell swirling motion (1) can be generated during migration of strongly connected cell clusters through dense environment made by cells in passive (resting) state during a tissue development [9] and (2) have been observed during migration of the internal cell group within a Neural crest supracell caused by contractions of an actin cable [18, 19]. Propagative waves could be generated during collective cell migration of stratified epithelium under *in vivo* conditions [18].

The rheological behavior of a matrix influences cell–cell and cell–matrix interactions and through the viscoelastic force influences the rate of cell spreading, as well as characteristics of generated mechanical waves.

CONCLUSION

Oscillatory instabilities in the form of mechanical waves are generated during collective cell migration such as propagative waves and standing waves. The propagative waves are generated during monolayer free expansion, whereas standing waves are generated during cell swirling motion of a confluent monolayer. Significant attempts have been made to describe the main characteristics of mechanic waves. The main characteristics of standing waves are (1) the radial velocity and cell tractions are uncorrelated; (2) radial stress component σ_{crr} and the corresponding strain rate $\dot{\epsilon}_{crr}$ are uncorrelated; (3) radial stress component is simultaneously tensional and compressional; and

(4) time derivative of the stress component is in a phase with the corresponding strain rate. The main characteristic of propagative waves is that (1) normal stress component σ_{cxx} and corresponding strain rate $\dot{\epsilon}_{cxx}$ are in phase quadrature; (2) normal stress component is always tensional; and (3) velocity and cell tractions are uncorrelated. However, a little is reported about the influence of the monolayer viscoelasticity on generation of mechanical waves. Mechanical waves have recognized during flow of various viscoelastic systems under low R_e number. The phenomenon is called the elastic turbulence. The elastic turbulence has been quantified by the ratio between two dimensionless parameters such Weissenberg number and Reynolds number. These oscillatory flow instabilities have also been monitored experimentally during 2D collective cell migration.

Propagative waves represent the consequence of cell forward flow and cell backward flow during monolayer expansion driven by interrelation between forces such as the viscoelastic force, the traction force, and the surface tension force. These forces influence the rate of change of momentum and lead to periodic extensions in the direction of flow. Standing waves represent the consequence of cell radial inflow and outflow during swirling motion driven by the interrelation between the centrifugal force, the viscoelastic force, and the traction force, while the influence of the surface tension force can be neglected. This force balance leads to the periodic extension and compression in the direction perpendicular to flow. The apparent inertial effects represent the characteristic of (1) the backward flow during monolayer free expansion and (2) the inflow during the cell swirling motion within a confluent monolayer.

Additional experiments are necessary in order to determine a long-time constitutive model for 2D multicellular systems caused by collective cell migration and correlate the migrating patterns with the residual stress distribution and the rate of its change. Cell long-time rearrangement can be controlled by matrix viscoelasticity. This theoretical consideration could help in deeper understanding of various biological processes by which an organism develops its shape and heals wounds in the context of the mechanism underpinning the epithelial expansion.

AUTHOR CONTRIBUTIONS

IP-L: conceptualization, methodology, and writing—original draft preparation. MM: illustrations and writing—review and editing. All authors contributed to the article and approved the submitted version.

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Conflict of Interest: The authors declare that the research was conducted in the absence of any commercial or financial relationships that could be construed as a potential conflict of interest.

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